1	Comparing electronic probes for volumetric water content of low-density					
2	feathermoss.					
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12

### 12 ABSTRACT

13 Feathermoss is ubiquitous in the boreal forest and across various land-cover types of the 14 arctic and sub arctic. A variety of affordable commercial sensors for soil moisture content 15 measurement have recently become available and are in use in such regions, often in 16 conjunction with fire-susceptibility or ecological studies. Electromagnetic sensors 17 available include frequency and time domain designs with variations in wave guide and 18 sensor geometry, the location of sensor electronics and operating frequency. Few come 19 supplied with calibrations suitable or suggested for low bulk density soils high in 20 organics. We tested seven of these sensors (CS615, ECH2O, GroPoint, Vitel, Theta, 21 TDR, Watermark) for use in feathermoss. Sensors installed in live, dead and burned 22 feathermoss samples, drying in a controlled manner, were monitored continuously and 23 compared to gravimetric determinations of moisture content. Almost all of the sensors 24 tested were suitable for measuring the moss sample water content over a range of water 25 contents from dry to field capacity, and we present a unique empirical calibration for each 26 sensor for this material. Differences in sensor design lead to changes in sensitivity as a 27 function of volumetric water content. These differences will affect the spatial averaging 28 over the soil measurement volume. Sensitivity analysis shows that empirical calibrations 29 are required for different soil types.

### 30 INTRODUCTION

# 31 1.1 Electromagnetic Techniques for Measuring Volumetric Water Content

32 Since the 1960s, electromagnetic techniques have been studied and used for measuring 33 the volumetric water content of porous media. Most applications in the geosciences have 34 been in mineral soils, for which both empirical relationships (for example, Ledieu et al., 35 1986; Topp et al.; 1980, Stein and Kane 1983) and theoretical models (for example, Roth 36 et al., 1990) exist for estimating volumetric water content from the bulk relative dielectric 37 permittivity. A few empirical relationships exist for soils high in organic content 38 (Herkelrath et al., 1991; Roth et al., 1992), but not for mosses other than cultivated peat 39 derived from Sphagnum moss (Myllys and Simojoki 1996). Based on their review of calibration equations, Jacobsen and Schønning (1995) suggested that organic soils might 40 41 require special treatment.

42 Under the assumption that all moss tissue has a common dielectric constant, 43 differences in the bulk dielectric constant of mosses at the same volumetric water content 44 are due to differences in volumetric fractions of air and moss in the sampling volume, i.e. 45 to differences in bulk density and to differences in the distribution of water between 46 bound and free states. Moss differs from low bulk density soils in that the solid phase is 47 composed mostly of organics with highly polar surfaces and a significant portion of the 48 soil water is incorporated into the moss as inner-cellular solution, which may have a 49 different dielectric constant than that of free water. Both factors can be expected to 50 increase the proportion of water in a bound state relative to mineral soils with similar 51 characteristic particle size and therefore to decrease the apparent relative dielectric 52 permittivity of the bulk soil for a similar water content.

53 Assuming a representative volume element of soil, a general relationship between the real part of the dielectric permittivity,  $\phi$ , and the volumetric water content,  $\theta$ , should 54 exist for a porous medium with spatially homogeneous composition, porosity and texture. 55 56 In practice, however, the apparent relative dielectric permittivity of the medium is also 57 affected by sensor measurement frequency and geometry and medium structure, density, 58 and water content (Topp et al., 1980). An empirical calibration lumps together the 59 influences of the medium and of the sensor on the measurement. Most calibrations 60 presented in the literature deviate from Topp's relationship (Topp et al., 1980; for example, Jacobsen and Schønning, 1995) and soil texture is generally invoked as the 61 62 cause of the deviation. Attempts have been made to extend the applicability of TDR 63 calibration curves by soil characteristics such as bulk density (e.g. Malicki, 1989). In 64 practice, this will not eliminate the necessity of sampling the material, or similar 65 materials, in which water content measurements are to be carried out in order to create 66 suitable calibration curves.

67 More than 23 studies of the TDR technique in a wide variety of materials are available in the literature. Third-order calibration curves for peat moss, litter or soils high 68 69 in organic or measured carbon content are available from Herkelrath et al., (1991), 70 Ledieu et al., (1986), Myllys and Simojoki (1996), Pepin et al., (1992), Roth et al., 71 (1992), and Topp et al., (1980). Mineral soil calibrations (e.g. Dasberg and Hopmans, 72 1992; Jacobsen and Schønning, 1995; Ledieu et al., 1986; Malicki and Skierucha, 1989; 73 Nadler et al., 1991) predict higher relative dielectric permittivities for volumetric water contents above 0.4 m<sup>3</sup> m<sup>-3</sup>, consistent with the prediction made above. Below this value, 74 75 the regions bounded by organic and mineral calibrations overlap.

76 Sensor type influences the calibration through sensor geometry and frequency, 77 both of which affect the spatial weighting function applied to the soil volume (Ferré et al, 78 1996; Nissen et al., 2003; Zegelin et al., 1989). Both the measurement volume and spatial 79 weighting are dependent on sensor design (Ferré et al., 1996; Knight 1992; Zegelin et al., 80 1989; Pepin et al., 1992). Ferré et al (1996) showed that sensor output averages variations 81 in water content along the wave guides for uncoated wave guides but not for coated wave 82 guides. For all sensor designs, the soil volume proximal to the sensor wave guides is 83 more heavily weighted in averaging of the apparent relative dielectric permittivity. Thus, 84 the density of plant tissue immediately adjacent to the tines of the sensor exerts a 85 disproportionately large influence on sensor output. Thicker tined-sensors, which shift 86 and compact more of the solid soil matrix (moss tissue) on insertion may have a tendency 87 to change the character of this near-tine material to a greater degree, particularly in a low 88 bulk-density material.

89 Since TDR was developed and gained common usage as a means of measuring 90 volumetric soil water, numerous other devices exploiting the sensitivity of the relative 91 dielectric permittivity to soil water content have appeared on the market. They have the 92 advantage of being cheaper and simpler to employ than TDR. While TDR measurements 93 are only slightly influenced by the nature of the soil (Ledieu et al., 1986), most 94 inexpensive commercially available sensors, both time domain and capacitance, provide 95 calibrations relating sensor output directly to volumetric water content for use in a limited 96 number of media. As with the empirical relationships in the literature, none provide 97 calibrations with a finer distinction than mineral vs. organic soils.

98 Feathermoss is virtually ubiquitous in the boreal forest and common in higher 99 latitudes. Its presence is sensitive to changes in environmental conditions and particularly 100 to changes in water content. The water content of moss cover in both of these regions is 101 also important because it determines boreal forest fire susceptibility, and because the 102 thermal properties of the surface layers are highly sensitive to water levels (Yoshikawa et 103 al., 2003). The bulk thermal conductivity and heat capacity of this surface layer have 104 been shown elsewhere to play a pivotal role in controlling permafrost persistence or 105 degradation (Yoshikawa et al., 2003).

106 Feather mosses include species from a number of genera, all of which share 107 similar morphological characteristics, such as prostate growth habit and branched stems. 108 Dry bulk densities for feathermoss species have been reported in the literature (Table 1) and cover a range from 0.01 to 0.05 kg m<sup>-3</sup>. Feathermoss changes in bulk density within 109 110 live and decomposing layers, as well as generally over depth. As an indication of their 111 variability, values for dry bulk density from a number of sources are plotted with sample 112 depth in Figure 1. Higher dry bulk densities are recorded with greater depth, and reflect 113 the accumulation of dead moss tissue beneath the living layer.

In this paper, we test the suitability of a number of electromagnetic devices for measuring the volumetric water content of feathermoss. These sensors are used in feathermoss in Arctic (Romanovsky and Osterkamp, 2000; Hinkel et al., 2001) and sub-Arctic (Harden et al., 2004) soils. The differences between sensor calibrations and the influence of their design are important considerations when planning field measurements and when comparing data derived from different sensors or sensors measuring water content in differing materials. This has particular relevance to climate gradient and 121 remote-sensing studies that seek to compare results from different ecosystems or to 122 ground-truth spatially distributed data.

123 METHODS

Seven electronic sensors were tested and included two time domain reflectometry 124 sensors: the TDR100 (Campbell Scientific, Inc.) with the CS605 TDR probe and the 125 GroPoint (Environmental Sensors Inc.). Four capacitance (sometimes referred to as 126 127 frequency domain reflectometry or FDR) sensors were also included: the CS615 probe 128 (Campbell Scientific, Inc.), the ECH<sub>2</sub>O probe (Decagon device, Inc.), the Hydra Vitel 129 probe (Stevens Water Monitoring Systems Inc.), and the Theta ML2x Delta-T probe 130 (Delta-T devices, Inc.), as well as a device based on measured electrical resistance, the 131 Watermark sensor model 200SS (Irrometer Co.). Other than the latter device, each sensor has unique wave-guide geometry, frequency and electronics, details of which are given in 132 133 Table 2. The CS615, ECH<sub>2</sub>0, GroPoint, Hydra Vitel probe, Theta probe and carry on-134 board electronics, while the TDR probe is a simple wave-guide. The wave-guide 135 geometry is important for the ease of installation, disturbs the soil matrix on installation to different degrees and changes the soil volume over which the measurement is made. 136 137 Finally, the ECH<sub>2</sub>0 probe is unique among the electromagnetic sensors tested here, 138 because its tines are encased in a sensor board.

Methods were selected to demonstrate that the seven soil water sensors listed in Table 2 were effective in determining the water content of the live and dead part of feathermoss. Bulk samples of forest floor feathermoss were harvested in spring (May and June) from three locations around Fairbanks, Alaska (Birch Hill, University Ski Trails and Delta Junction). Each block contained a mix of feathermoss species, in each case

144 predominantly of *Pleurozium* and *Hylocomium* species. Both live and decomposing moss 145 was collected in each case. A sample of burned, partially charred moss from the Tanana 146 River flood plain, Alaska was also used for TDR calibration. The four feathermoss 147 samples were discriminated by layer (live or dead) and cut to known volume. Live and dead moss layers are usually distinguished on the basis of color, the presence of litter and 148 149 the relative proportion of fibric moss tissue. In practice, we found a division of lesser 150 cohesion between more loosely bound live moss tissue and the underlying, more tightly 151 matted dead moss tissue, which roughly corresponded to the division based on color. 152 Each layer was over 0.1 m thick.

153 The seven sensors were placed in the sample block in parallel orientation, 154 extending from the insertion side of the block into its interior. Feathermoss sample blocks were set in an upright position and allowed to soak for more than 24 hours before 155 156 measurements began. The saturated feathermoss samples, including sensors, were lifted 157 out of the water in mesh baskets, drained to approximately field capacity and weighed 158 during drying in a 30°C forced air oven using an electronic balance. Sensor cables were 159 supported to avoid their influence on the measured weight and the sensors remained 160 inserted in the samples for the duration of the experiment. Balance output was recorded 161 every 5 minutes. Temperature data within the oven and the moss samples was recorded 162 using thermistors at 5-minute intervals during the experiment. Sensor output was 163 measured simultaneously with all seven sensors at five-minute intervals during drying 164 until the sample block reached a stable weight over a twelve-hour period. The volume of 165 the sample block varied with water content and was estimated using its dimensions at a number of points during the drying process. 166

167 All sensor output signals were logged with a CR10X datalogger (Campbell 168 Scientific, Inc.). TDR waveforms were analyzed with a computer algorithm based on 169 Heimovaara and Bouten (1990), but including an endpoint determination algorithm that 170 accounts for signal attenuation with increased travel time. All waveforms were analyzed 171 visually, following the recommendations of Dasberg and Hopmans (1992). The Vitel 172 sensor outputs three voltages for soil water content determination and one for sensor head 173 temperature, so that temperature compensation to dielectric and conductivity values can 174 be performed. The manufacturer provides an algorithm for this compensation. The CS615 175 sensor outputs a single period measurement from which the bulk soil dielectric constant 176 may be calculated using an empirical polynomial calibration. The manufacturer-supplied 177 calibrations are for 20 ±C and a correction coefficient has been developed for 178 measurement temperatures of 10 to 30 ±C (Campbell Scientific, Inc., 1996). Output from the ECH<sub>2</sub>O (single voltage), GroPoint (single current) and Watermark (single resistance) 179 180 sensors were left untreated.

181

182 
$$t > \frac{L\sqrt{\phi}}{2}$$

С

183 where *t* is the travel time,  $\phi$  is the relative dielectric permittivity, *L* is the length of the 184 TDR wave guides and *c* is the speed of light in free space (2.997  $\propto 10^8$  m s<sup>-1</sup>). For the 185 CS615 sensor, the measured response is a period from which the bulk dielectric constant 186 may be calculated:

For TDR, the measured travel time of the is related to the permittvity:

187 
$$\upsilon > 2\left(t_{cir}, \frac{2L\sqrt{e}}{c}\right)$$

188	where v is the period output, $t_{cir}$ is delay of the circuit components, L is the probe length,
189	c is the speed of light. The Vitel Hydraprobe is delivered with binary versions of
190	proprietary software that calculates soil water content from 3 sensor output voltages and
191	sensor temperature from the fourth voltage. Output values include the real and imaginary
192	parts of the soil dielectric constant, the soil conductivity, water content and temperature.
193	We make the assumption that the sensor response is accurately represented by the
194	calculated real part of the dielectric constant before temperature correction. The Delta-t
195	Theta probe operation has been described by Miller and Gaskin (1999). The measured
196	quantity for the sensor in a datalogging mode is a voltage for which Delta-t provides a
197	linear and a cubic calibration to relative dielectric permittivity:

198  $\sqrt{\phi} > 4.44$ V, 1.10

199 and:

200  $\sqrt{\phi} > 4.70 \text{V}^3$ . 6.40 V<sup>2</sup>, 6.40 V, 1.07

where V is the sensor output voltage. The linear relationship is used for calibrations relating the dielectric constant and volumetric water content. Similarly, the ECH<sub>2</sub>O form of the empirical calibration suggested by the manufacturer is a linear relationship between sensor output voltage and volumetric water content. GroPoint sensors are not delivered with an algorithm for calculating dielectric constant from sensor output, but a linear function is applied to the current output of the device.

207

# 208 **RESULTS AND DISCUSSION**

209 Calibrations

210 For all probes, excepting the Watermark, calibration curves were generated relating the 211 gravimetrically-determined volumetric water content to sensor output over a range of 0.025 - 0.15 m<sup>3</sup> m<sup>-3</sup> for live moss tissue and from 0.025 - 0.20 m<sup>3</sup> m<sup>-3</sup> for dead moss 212 213 tissue. Figure 2 shows these results except for the Watermark sensor. The given 214 volumetric water contents range from near field capacity to air-dry values. The field capacities for the live, dead and burnt mosses were approximately 0.15, 0.20 and 0.20  $\text{m}^3$ 215 m<sup>-3</sup>, respectively. The rapid change in water content on removal of the sample block from 216 217 the water hampered the determination of field capacity and of the bulk dielectric at water 218 contents near field capacity. In practice, the field capacity depends on the nature of the underlying material. Least squares 2<sup>nd</sup> or 3<sup>rd</sup> order polynomial fits of the data for each of 219 the sensors, excepting the Watermark, were performed. The polynomial coefficients and 220 221 correlation coefficients are listed in Table 3, along with the probe output domain, 222 expressed as a range of dielectric constant or sensor output values, for each relationship.

The Watermark sensor output decreased measurably up to volumetric water contents of 5% and 7% for live and dead moss, respectively. At higher water contents, the probe output is essentially independent of changes in water content. The Watermark probe distinguishes between the air-dry and near-saturated states of the moss.

The differences between sensor outputs under similar dielectric constant conditions suggest that the volume of sensitivity, which is the volume of bulk sample over which the probe measures a spatially weighted average dielectric constant, and spatial weighting within this volume, affected sensor output. For all of the sensors, sample volume proximal to the sensor tines is heavily weighted. Sensor insertion into the sample displaces moss. In contrast to mineral soil matrices, compression of the moss

around the sensor causes a localized increase in bulk density proximal to the sensor tines. 233 234 Although the range of tine diameters for the sensors presented here is small (2.5 to 6 235 mm), this effect would to an underestimate of water content increasing with tine 236 diameter. Ferré (1996) showed that such effects are not independent of tine spacing, 237 diameter and coating and of heterogeneities in the distribution of water around the sensor 238 itself. Sensor dimensions play a larger role in moss than in mineral soils due to probe 239 contact and air void effects, particularly for sensors using lower measurement frequencies 240 than TDR, at which the apparent dielectric permittivity is more sensitive to bulk density 241 (Hallikainen et al., 1985).

242 The question facing someone using any of these sensors in moss is what sort of 243 calibration is necessary and sufficient to achieve a particular uncertainty. One can choose 244 between calibrating for the specific material into which the sensor is to be installed, 245 which is appropriate to permanent installation in a particular soil horizon. If the sensor is 246 to be used in a handheld fashion in the field inserted from the surface, however, a wider 247 range of materials will need to be included in the calibration. Based on the data presented 248 here, we recommend separate calibrations for live and dead horizons, i.e. for differing 249 stages of decomposition.

The feathermoss TDR calibrations presented here lie within the range of the low bulk density and organic media calibrations listed in the Introduction. The TDR graph of Figure 2 includes data for a block of charred dead feathermoss. This sample was dark, brittle and dusty, with a bulk density of over 0.12 kg m<sup>-3</sup> for a 10 1 sample. The TDR calibration curves suggests that burning feathermoss changes the apparent dielectric constant of the moss, presumably as a result of changes in the moss structure and perhaps the formation of carbon deposits. In this study, live and dead moss output values approached each other at low water contents, but diverged with increasing water content. Probe output, or measured dielectric constant, was lower for live feathermoss than for dead at most volumetric water contents, for all tested probes except the ECH<sub>2</sub>O and the GroPoint sensors, for which sensor output values for live and dead moss were closer than  $\pm 6\%$  (20 mV). This is generally consistent with the difference in bulk densities (live 0.022; dead 0.06 kg m<sup>-3</sup>) observed.

263

## 264 **RECOMMENDATIONS**

265 We present calibration curves for six sensors in live and dead feathermoss. For all six, calibration curves for the calculation of volumetric water content from measured 266 dielectric constant or sensor output, depending on sensor type, were created in live and 267 dead feathermoss over a volumetric water content range of approximately 0.02 to 0.2 m<sup>3</sup> 268 m<sup>-3</sup>. Calibration in multiple samples of the medium in which each sensor is to be used is 269 270 advocated, whereby the uncertainty in the calibration is probably affected by spatial 271 variability of the moss bulk density. The selection of samples for calibration should be 272 determined by the intended use of the sensor. Sensor output in live and dead feathermoss 273 layers at the same volumetric water content differ by more than 10% measured water 274 content. Site-specific calibrations must therefore also record the horizons in which the 275 sensors are being used, a consideration relevant to measurements made from the ground 276 surface.

277

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383

383 List of Tables

**Table 1.** Bulk density ranges for feather and *Sphagnum* mosses from the literature.

**Table 2.** The physical and operating characteristics of the sensors.

**Table 3.** Calibration coefficients for relating sensor output or measured dielectric to

387 volumetric water content in live and dead feathermoss. The coefficients for the

388 expression:

389 volumetric water content = a x + b,

390 are given, where x is either sensor output or the square root of the dielectric constant, as

391 listed in Table 2. The range of sensor output or dielectric constant for which the sensors

392 were calibrated in feathermoss is given the rightmost columns (units are listed in Table

393 2).

394 List of Figures

**Figure 1.** Bulk density as a function of depth for live and dead feathermoss layers from

- 396 Delta Junction, Alaska Manies et al.; Manitoba, Canada O'Neill et al., (1995) and the
- 397 Frostfire experiment in Alaska Harden et al., (2004).
- 398 Figure 2. Variation in measured dielectric constant (CS615, TDR, Theta and Vitel
- sensors) or sensor output (ECH<sub>2</sub>O and GroPoint) with volumetric soil water content for
- 400 six sensors for live and dead feathermoss. The TDR graph shows additional data from a
- 401 sample of charred feathermoss.



Figure 1.



	Bulk density [kg m <sup>-3</sup> ]				
sample	live	dead			
	(# samples)	(# samples)			
Feather moss species dry	$0.013(6)^{\dagger}$	<b>0.049 (6)</b> <sup>†</sup>			
bulk density	<b>0.019</b> (6) <sup>‡</sup>	0.041 (8) ‡			
	0.040 (27) <sup>§</sup>	<b>0.092</b> (7) <sup>§</sup>			
	0.022 (23) ¶	0.06 (1) ¶			
Sphagnum		0.108#			
dry bulk density		$0.8-100^{\ddagger\ddagger}$			
v	0.0129 - 0.0314 <sup>§§</sup>				
	0.0168 - 0.0406 <sup>§§</sup> (capitulum				
	0.019 – 1.40 (corresponding				

mat thicknesses of 3 - 47 cm) <sup>§§</sup>

† - Trumbore et al. (1999); ‡ - King et al. (2002);
§ - O'Neill et al. (1995); ¶ - this study; # Yoshikawa et al. (2004); ‡‡ - Yoshikawa et al.
(2003); §§ - Kane et al. (1978).

Table 1.

	Sensor	Characteristics			Dimensions [mm]		
type		frequency [MHz	] wave shape	sensor output	sensor length	tine diameter	tine spacing (#)
	CS615	55.5	sine	<b>1 pulse</b> [700 - 1400 ms]	288	3.2	28.5 (2)
Time Domain	GroPoint	2 (0.5 microns)	pulse	<b>1 current</b> [0-5 mA]	205	6	25 (2)
	TDR100	3000 (130 ps)	pulse	<b>waveform</b> voltage <i>vs</i> . time	300	4.8	22 (3)
	ECH <sub>2</sub> O	2 (pulse)/6 (sine)	pulse/sine	<b>1 voltage</b> [400-1000 mV]	200	2.5/7.5	6 (3)
Frequency Domain	Theta	100 MHz	sine	<b>1 voltage</b> [<1000 mV]	59	3.2	10 (2)
	Vitel	50 MHz	sine	4 voltages [<2500 mV]	57	4	8.6 (4)
Electrical Resistance	Watermark	DC		<b>1 resistance</b> [0.1-500 kΩ]	70	22.5	

sensor	moss	coefficie	0	main $^{\dagger}$		
		a	b	$\mathbf{R}^2$	X <sub>min</sub>	<b>x</b> <sub>max</sub>
CS615	dead	$6.99 \ge 10^{\circ}$	9.80 x 10 <sup>-1</sup>	0.981	1.18	1.58
	live	$4.88 \ge 10^{\circ}$	9.84 x 10 <sup>-1</sup>	0.966	1.14	2.63
ECH <sub>2</sub> O	dead	$5.00 \ge 10^{-1}$	$2.58 \ge 10^{-1}$	0.937	270	357
	live	$6.58 \ge 10^{-1}$	$2.52 \times 10^{-1}$	0.975	264	384
GroPoint	dead	$5.92 \ge 10^{\circ}$	$1.00 \ge 10^{-2}$	0.996	0.02	1.70
	live	6.69 x 10 <sup>0</sup>	8.08 x 10 <sup>-2</sup>	0.994	0.02	1.55
TDR	dead	$1.55 \ge 10^1$	6.83 x 10 <sup>-1</sup>	0.997	1.04	1.96
	live	$8.05 \ge 10^{\circ}$	7.46 x 10 <sup>-1</sup>	0.929	1.02	3.67
	burnt	$2.69 \ge 10^{\circ}$	$1.77 \ge 10^{0}$	0.983	1.86	2.34
Theta	dead	$1.90 \ge 10^1$	$5.80 \ge 10^{-1}$	0.995	2.40	5.80
	live	$9.22 \ge 10^{\circ}$	$1.10 \ge 10^{0}$	0.998	1.18	16.8
Vitel	dead	$1.31 \ge 10^1$	8.98 x 10 <sup>-1</sup>	0.993	1.70	2.43
	live	$8.05 \ge 10^{\circ}$	$1.32 \ge 10^{\circ}$	0.989	1.37	3.39

† – sensor outputs and units are listed in Table 2.