



## The Relevance of Grain Dissection for Grain Size Reduction in Polar Ice: Insights from Numerical Models and Ice Core Microstructure Analysis

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The flow of ice depends on the properties of the aggregate of individual ice crystals, such as grain size or lattice orientation distributions. Therefore, an understanding of the processes controlling ice micro-dynamics is needed to ultimately develop a physically based macroscopic ice flow law. We investigated the relevance of the process of grain dissection as a grain-size-modifying process in natural ice. For that purpose, we performed numerical multi-process microstructure modeling and analyzed microstructure and crystallographic orientation maps from natural deep ice-core samples from the North Greenland Eemian Ice Drilling (NEEM) project. Full crystallographic orientations measured by electron backscatter diffraction (EBSD) have been used together with c-axis orientations using an optical technique (Fabric Analyser). Grain dissection is a feature of strain-induced grain boundary migration. During grain dissection, grain boundaries bulge into a neighboring grain in an area of high dislocation energy and merge with the opposite grain boundary. This splits the high dislocation-energy grain into two parts, effectively decreasing the local grain size. Currently, grain size reduction in ice is thought to be achieved by either the progressive transformation from dislocation walls into new high-angle grain boundaries, called subgrain rotation or polygonisation, or bulging nucleation that is assisted by subgrain rotation. Both our time-resolved numerical modeling and NEEM ice core samples show that grain dissection is a common mechanism during ice deformation and can provide an efficient process to reduce grain sizes and counter-act dynamic grain-growth in addition to polygonisation or bulging nucleation. Thus, our results show that solely strain-induced boundary migration, in absence of subgrain rotation, can reduce grain sizes in polar ice, in particular if strain energy gradients are high. We describe the microstructural characteristics that can be used to identify grain dissection in natural microstructures.

Keywords: ice microstructure modeling, cryo-ebsd, fabric analyser, ice deformation, dynamic recrystallization, grain size evolution, grain dissection, neem ice core

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## INTRODUCTION

Knowledge of the properties and processes controlling the flow of ice is essential to understand ice sheet dynamics. Ice sheets creep under gravitational forces (Petrenko and Whitworth, 1999) and their macroscopic flow is affected by properties of individual ice crystals, such as crystallographic preferred orientation (CPO) and grain size (Bader, 1951; Steinemann, 1954; Budd and Jacka, 1989; Van Der Veen and Whillans, 1990; Mangeney et al., 1997; Ng and Jacka, 2014). Ice crystals in ice sheets are thought to mainly accommodate deformation by viscoplastic glide and climb of intracrystalline lattice defects, which is known as dislocation creep (Shoji and Higashi, 1978; Pimienta and Duval, 1987). On Earth, the only stable ice polymorph is hexagonal ice Ih, which has a significant viscoplastic anisotropy. The glide resistance on the basal plane, which is perpendicular to the c-axis, is at least 60 times lower than that on the prismatic and pyramidal glide planes (Duval et al., 1983). With deformation, c-axes align in the direction of maximum finite shortening (Azuma and Higashi, 1985) causing a macroscopic mechanical anisotropy of the polycrystalline aggregate (Gao and Jacka, 1987; Budd and Jacka, 1989).

Dislocation creep depends on the CPO and is grain size insensitive. However, other deformation mechanisms such as *grain boundary sliding* or *diffusion creep* are known to depend on grain sizes (Raj and Ashby, 1972; Shoji and Higashi, 1978) and may be strain rate controlling at low stresses (Goldsby and Kohlstedt, 1997, 2001; Pettit and Waddington, 2003). An understanding of grain size evolution in ice sheets including all relevant processes and proposed models (Durand et al., 2006; Ng and Jacka, 2014) is essential to include the full suite of deformation mechanisms into ice flow modeling.

In various deep ice cores, grain size is observed to increase with depth until a stable value is reached (Li et al., 1998; Montagnat et al., 2012; Fitzpatrick et al., 2014). Where drill cores penetrate the glacial to Holocene transition, a distinct decrease in grain size and increase in CPO strength is found (Faria et al., 2014a; Montagnat et al., 2014; Weikusat et al., 2017a and references therein). The North Greenland Eemian Ice Drilling (NEEM) ice core reflects this typical microstructural evolution. In NEEM, a relatively stable grain size of about 10 to 12 mm<sup>2</sup> is observed below a depth of ca. 400 m, but the CPO progressively strengthens further down (Kipfstuhl, 2010; Weikusat and Kipfstuhl, 2010; Binder, 2014; Montagnat et al., 2014). A distinct change toward strongly aligned c-axes that form an elongated, vertical single maximum is observed at the transition from Holocene to glacial ice at 1,400 m depth (Binder, 2014; Montagnat et al., 2014). In the glacial ice, the grain sizes are smaller and more variable than in Holocene ice. This is observed to correlate with higher impurity load in glacial ice. However, the relation of grain size and CPO with impurities is still under discussion (Eichler et al., 2017).

The grain size in ice results from a combination of grain growth and grain-size-reducing mechanisms. The downward increase in grain size in shallow ice toward stable grain sizes implies a stronger relative contribution of grain-sizereducing mechanisms when stable grain sizes are achieved. As ice in ice sheets mostly deforms at temperatures close to its pressure melting point, recrystallization is expected to accompany viscoplastic deformation (Duval, 1979; Jacka and Li, 1994; Kipfstuhl et al., 2009). Recrystallization includes rotation of crystal lattices, as well as grain boundary migration and/or formation of new grain boundaries (Faria et al., 2014b).

The migration of grain boundaries during normal graingrowth (NGG) is driven by surface energy minimisation (Smith, 1964; Weaire and Rivier, 1984; Duval, 1985; Alley et al., 1986a,b; De La Chapelle et al., 1998). NGG leads to an increase of mean grain area with time and equidimensional grains with slightly curved grain boundaries forming 120° angles at grain boundary triple junctions. Strain-induced boundary migration (SIBM), however, is driven by strain energies that result from the elastic lattice distortion caused by dislocations (Humphreys and Hatherly, 2004, pp. 251-253). During SIBM, grain boundaries migrate toward highly strained areas in adjacent grains and leave behind dislocation-free regions. This usually causes irregular grain boundaries and bulges toward high-energy regions (Means, 1981). SIBM in ice is assumed to cause increasing grain sizes (Duval and Castelnau, 1995) and has been termed dynamic graingrowth when combined with NGG (Urai and Jessell, 2001; Faria et al., 2014a,b).

During recovery, dislocations arrange in lower energy configurations (White, 1977; Urai et al., 1986). This leads to the gradual transformation of low-angle dislocation walls into subgrain boundaries (Weikusat et al., 2017b) and eventually into new high-angle grain boundaries. This process of rotational recrystallization or *polygonisation* leads to a grain size reduction (Alley et al., 1995; Roessiger et al., 2011). The formation of new grains by spontaneous nucleation is a further mechanism of grain-size reduction, but is thought to be very unlikely in the absence of strong chemical driving forces, as is the case for ice (Drury and Urai, 1990; Humphreys and Hatherly, 2004; Faria et al., 2014b). During bulging nucleation, small grains separate from the serrated grain boundary formed by SIBM assisted by subgrain rotation. Bulging nucleation is suggested to reduce grain sizes in ice (Duval and Castelnau, 1995; De La Chapelle et al., 1998; Montagnat et al., 2015) and is observed in creep tests on columnar ice at high temperatures and stresses (Chauve et al., 2017). The deformation-induced recrystallization mechanisms (SIBM, polygonisation and nucleation) are together termed dynamic recrystallization. Of these mechanisms, SIBM and polygonisation are thought to be dominant in glaciers and ice sheets.

While bulging recrystallization driven by SIBM assisted by other processes can reduce grain sizes in ice, SIBM in isolation is generally assumed to result in a grain-size increase in glaciology. However, SIBM has been observed to decrease grain size in deformation experiments on rock analogs by Means (1983, cf. Figure 4 therein) and Urai (1983, cf. Figure 14 therein). Both studies observed SIBM with rapidly migrating bulges, eventually migrating through a grain and splitting it into two parts when reaching an opposite grain boundary. This causes an effective mean grain-size reduction by forming two "new" grains with similar CPO. Resulting groups of grains with similar orientation were called "orientation families" by Urai (1983). This process was termed *grain dissection* by Urai et al. (1986) and Urai (1987) is known as *geometric dynamic recrystallization* in metallurgy (Humphreys and Hatherly, 2004, pp. 461–465; De Meer et al., 2002; **Figure 1**). Grain dissection is readily observed, if timeresolved microstructure evolution is available, corresponding movies of grain dissection in rock analogs are presented by Urai and Humphreys (2000). Grain dissection is only effective when the grain size is similar to the size of grain-boundary bulges. At larger grain sizes, bulges cannot reach the other side of a grain and polygonisation or bulging nucleation would dominate. At smaller grain sizes, bulges sweep over a whole grain and thus remove it, which leads to a mean grain-size increase. It follows that grain dissection is most effective at a stable grain size, when polygonisation and grain dissection operate in conjunction.

Grain dissection has not yet been explicitly observed in natural ice microstructures. Breton et al. (2016) report grain dissection in deformation experiments on laboratory-prepared ice and suspect a grain-size-reducing character. So far, it is assumed that stable grain sizes in ice are achieved by an interplay of dynamic graingrowth, polygonisation and potentially nucleation processes (Alley et al., 1995; De La Chapelle et al., 1998; Montagnat and Duval, 2000; Mathiesen et al., 2004; Roessiger et al., 2011; Chauve et al., 2017; Hidas et al., 2017). However, in rock analogs and bischofite, grain dissection is observed as an effective grain-sizereducing process, in particular at steady-state grain sizes (Jessell, 1986; Urai, 1987).

In this study, we investigate whether grain dissection is a relevant process during ice microdynamics. We consider the role of grain dissection in the grain size evolution in glacier/ice sheet ice and assess under which conditions it can potentially be an efficient grain-size-reducing mechanism. We use two approaches: (1) micro-dynamical modeling using the Elle microstructure-modeling platform coupled to a full-field crystal viscoplasticity code (VPFFT) and (2) microstructure and crystallographic orientation maps of natural ice. We use natural ice samples from NEEM ice core as it represents microstructural behavior typical for various other ice cores and a sufficiently large microstructural dataset from NEEM ice core is readily available. We denote ice deposited in the last glacial period, i.e. after Eemian, but before Holocene, "glacial ice" and ice deposited in the Holocene "Holocene ice."

### METHODS

### Microstructural Modeling The Elle Modeling Platform

The open-source numerical modeling platform Elle (Jessell et al., 2001; Bons et al., 2008; Piazolo et al., 2010) is optimized to model coupled or interacting microstructural processes. Elle was applied in various studies on ice microstructures, such as single and polyphase grain-growth (Roessiger et al., 2011, 2014). The full-field crystal viscoplasticity code (VPFFT) by Lebensohn (2001) coupled to Elle was used to simulate strain localisation, dynamic recrystallization and folding in ice with and without air bubbles (Bons et al., 2016; Jansen et al., 2016; Llorens et al., 2016a,b; Steinbach et al., 2016).

Here, only the essentials of the modeling approaches for deformation and recrystallization are summarized. For more detail on the principles of Elle, the reader is referred to Jessell et al. (2001) and Bons et al. (2008), for the VPFFT code to Lebensohn (2001), and for the coupling of both codes to Griera et al. (2013). Details on the grain boundary migration and recovery codes are presented in Becker et al. (2008) and Borthwick et al. (2014), respectively. The Elle/VPFFT algorithms to model dynamic recrystallization can be found in Llorens et al. (2016a) and Steinbach et al. (2016). If not indicated differently, we used previously published input parameters for our numerical models (see Llorens et al., 2016a,b; Steinbach et al., 2016). The basic simulation setup is summarized in **Table 1**, whereas **Table 2** contains more detailed information on the input parameters.

#### Microstructure Discretisation

In Elle, the two-dimensional microstructure of polycrystalline ice is discretised in a set of contiguous polygons, called *flynns*, in a cell with fully wrapping and periodic boundaries. The *flynns* are defined by straight boundaries than link boundary nodes (*bnodes*) in either double- or triple junctions. The *bnodes* are successively moved to achieve grain boundary migration.





TABLE 1   Ov	erview of the	settings of th	ne numerical	simulations.
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Simulation name	Initial number of grains	Initial mean grain area (mm <sup>2</sup> )	Numerical strain rate (s <sup>-1</sup> )
G05R10	2003	4.99	2 10 <sup>-10</sup>
G10R10	1000	10.00	2 10 <sup>-10</sup>
G15R10	667	14.99	2 10 <sup>-10</sup>
G20R10	500	20.00	2 10 <sup>-10</sup>
G30R10	333	30.03	2 10 <sup>-10</sup>
G40R10	250	40.00	2 10 <sup>-10</sup>
G60R10	167	59.88	2 10 <sup>-10</sup>
G80R10	125	80.00	2 10 <sup>-10</sup>
G05R11	2003	4.99	2 10 <sup>-11</sup>
G10R11	1000	10.00	2 10 <sup>-11</sup>
G15R11	667	14.99	2 10 <sup>-11</sup>
G20R11	500	20.00	2 10 <sup>-11</sup>
G30R11	333	30.03	2 10 <sup>-11</sup>
G40R11	250	40.00	2 10 <sup>-11</sup>
G60R11	167	59.88	2 10 <sup>-11</sup>
G80R11	125	80.00	2 10 <sup>-11</sup>

Each simulation is labeled with the initial mean grain-area in  $mm^2$  (G) and with the strain rate with R10 and R11 standing for  $2 \cdot 10^{-10}$  and  $2 \cdot 10^{-11}$  s<sup>-1</sup>, respectively. All simulations were repeated three times to average the number of grain dissection and polygonisation events.

During grain boundary migration, the development of quadruple or higher-order *bnode* junctions is not allowed, as well as island *flynns* with only one surrounding neighbor *flynn*. To store intracrystalline properties, such as crystal orientation, local stresses, strain rates or dislocation densities, a set of unconnected nodes (*unodes*) is superimposed on the *flynn* network. For our simulations, the *unodes* are arranged in a regular grid of  $256 \times 256$  *unodes*, which is a requirement of VPFFT. Crystal orientations are mapped onto *unodes* using Euler triplet angles following the Bunge convention (Bunge, 1982).

Topology checks are carried out at all times during the simulations to ensure compliance with topological restrictions (see **Figure 2**). The topology checks maintain the resolution defined by the set minimum (0.5 mm) and maximum (1.1 mm) *bnode* separation. A new topological check allows for grain dissection: Two unconnected (non-neighboring) double-junction *bnodes* are merged if they approach closer than the set minimum separation (**Figure 2**, c). This effectively splits the *flynn* adjacent to both *bnodes*, into two daughter *flynns*, which constitutes a grain dissection event. A dissection is not performed if less than three *bnodes* are between the two non-neighboring *bnodes*, as this would lead to an unviable daughter *flynn* (**Figure 2**, d). The number of dissection events is tracked throughout the simulation.

## Modeling Crystal Viscoplasticity and Dynamic Recrystallization

The full-field crystal viscoplasticity code (VPFFT) is based on calculating the stress field from kinematically admissible velocity fields that minimizes the average local work-rate under compatibility and equilibrium constraints (Lebensohn,

Symbol	Explanation	Input value
D <sub>min</sub>	Minimum bnode separation	$5 \times 10^{-4} \text{ m}$
D <sub>max</sub>	Maximum bnode separation	$1.1 \times 10^{-3} \text{ m}$
$\Delta t_{DRX}$	Time step for one recrystallization loop	$1.25 \times 10^7 s$
Ν	Number of recrystallization loops per one step of VPFFT within one simulation step for high and (low) strain rate setups	2 (20)
€incr	Incremental strain per simulation step	0.01
τ <sub>basal</sub> τ <sub>non-basal</sub>	Ratio non-basal/basal glide resistance (Llorens et al., 2016a,b; Steinbach et al., 2016)	20
M <sub>0</sub>	Intrinsic mobility grain boundary migration (Nasello et al., 2005)	$0.023 \text{ m}^4 \text{ J}^{-1} \text{ s}^{-1}$
Mr	Rotational mobility used for recovery code (Llorens et al., 2016a)	5.5 × 10 <sup>-7</sup> Pa <sup>-1</sup> s <sup>-1</sup> m <sup>-2</sup>
Ysurf	Ice grain interface surface energy (Ketcham and Hobbs, 1969)	0.065 J m <sup>-2</sup>
Eline	Energy per meter of dislocation for basal plane dislocations (non-basal energy can be up to about four times higher) (Schulson and Duval, 2009)	$3.6 \times 10^{-10} \text{ Jm}^{-1}$
α <sub>HAGB</sub>	Critical misorientation for high-angle grain boundary (HAGB) (Weikusat et al., 2011a,b; Steinbach et al., 2016)	5 °

**TABLE 2** Overview of crucial input parameters used for the numerical simulations.

Parameters where chosen to be consistent with published literature using similar numerical simulations or experimental data.

2001; Lebensohn et al., 2009; Griera et al., 2013). VPFFT assumes intracrystalline deformation in ice Ih accommodated by dislocation glide on basal, pyramidal and prismatic slip systems. The non-linear viscous, rate-dependent flow law predicts the strain rate and stress at each point in the computational grid defined by unodes. The non-basal slip resistance is set 20 times higher than for basal slip (**Table 2**) as a compromise between accuracy and computational efficiency. Systematic trial simulations for the studies by Llorens et al. (2016a,b, 2017) and Steinbach et al. (2016) showed that with the use a ratio of 20 instead of 60 does not significantly alter the microstructural evolution. A significant effect on the number of grain dissection events is therefore considered unlikely.

Since the strain rate and stress fields are initially unknown, VPFFT uses an iterative spectral solver based on the Fast Fourier Transformation. VPFFT computes the viscoplastic response for a short time-step during which velocities are assumed constant. The updated lattice orientations are remapped onto the rectangular *unode* grid and the displacement field is applied to all *bnodes*. Furthermore, geometrically necessary dislocation-densities are calculated by means of the plastic-strain gradient following Brinckmann et al. (2006). Following Gao et al. (1999), the plastic strain gradient is calculated from the partial



**FIGURE 2** | Microstructure discretisation and topological events necessary if *bnodes* move due to deformation or grain boundary migration. Insertion (a) and deletion (b) of a *bnode* to keep a constant resolution (c) Merging two non-neighboring *bnodes*, this numerically defines grain dissection (d) Insertion of new grain boundary by polygonisation between *unode* clusters above a critical misorientation (e) No merging of two non-neighboring *bnodes* as number of other *bnodes* between the two close *bnodes* is < 3 (f) Deletion of small *flynn* containing no *unodes* (g) Neighbor switch in triple *bnodes*.

derivatives of the plastic strain tensors, which are calculated by VPFFT.

The strain energy at a given position is a function of the dislocation density  $\rho$  and the dislocation line energy  $E_D$ , which is proportional to square of the Burgers' vector length of the respective dislocation type (Humphreys and Hatherly, 2004, pp. 17–18). In ice Ih, the Burgers' vector of non-basal dislocations is approximately two times longer compared to basal ones (Hondoh, 2000). Hence, non-basal dislocations can provide about four times higher strain energies. Previous numerical models by Llorens et al. (2016a,b) and Steinbach et al. (2016) assume all dislocations are on basal planes and at constant Burgers' vector length, which underestimates strain energies. Here, we use an updated approach that scales the strain energies to the non-basal activity in each *unode* which is predicted by VPFFT to allow up to about four times higher strain energies due to the presence of non-basal dislocations.

Following each VPFFT step, recrystallization is modeled using Elle. Each recrystallization step comprises successive steps of discrete implementations of grain boundary migration, recovery and polygonisation. Each mechanism is modeled using a fixed numerical time step and temperature (see section Simulation Setup; **Tables 1**, **2** for input parameters). For numerical stability reasons, the order in which the discrete implementations are performed on the numerical microstructure is first polygonisation, followed by grain boundary migration and recovery. This loop is repeated until the numerical time for the recrystallization processes equals the one envisaged for one deformation increment by VPFFT, which determines the numerical strain rate (see Steinbach et al., 2016 and **Figure 2** therein). As the numerical time steps and the resulting microstructural changes per step are low, we assume that the effective microstructural response is not significantly different from conditions during which the mechanisms operate concurrently.

Grain boundary migration is modeled using a front-tracking approach moving individual bnodes toward lower energy positions (cf. Becker et al., 2008; Llorens et al., 2016a). In this energy minimisation approach, the bnode displacement is calculated from multiplying its velocity with a fixed time step (section Simulation Setup; Table 2). The bnode velocity is proportional to the grain boundary mobility and driving force. The temperature dependant mobility is calculated following Nasello et al. (2005) by using an Arrhenius term with an experimentally derived intrinsic mobility and activation energy. The driving force is calculated from the change in local surfaceand strain-energy that result from a change in position of that bnode. These energy fields are determined with four trial positions close to the actual bnode position. The change in surface energy is due to a change in length of the grain-boundary segments to neighboring *bnodes*. The change in strain energy results from reducing the strain energy to zero in the area swept by the *bnode* and its adjoining boundary segments.

For the recovery mechanism, an energy minimisation approach is used that, analogous to the grain-boundary migration approach, calculates the lattice re-orientation with a rotational mobility term (Moldovan et al., 2001; Borthwick et al., 2014; Llorens et al., 2016a). The approach is based on decreasing the lattice misorientation between two unodes toward a lower energy configuration (see Borthwick et al. (2014) and Llorens et al. (2016a) for details). Recovery reduces the local dislocation density proportional to the decrease in lattice misorientation and allows the development of subgrains. The subgrains are defined as unode clusters with a certain minimum misorientation with neighboring clusters. The polygonisation routine detects these clusters and adds new high-angle grain boundaries defined by bnodes, if the cluster misorientation is above a critical angle. This is done by Voronoi decomposition of the unode clusters using the Voronoi points surrounding the cluster as new bnodes (Steinbach et al., 2016). We use a critical angle of  $5^{\circ}$  to be consistent with both published numerical studies (Steinbach et al., 2016; Llorens et al., 2017) and subgrain boundary quantifications by Weikusat et al. (2011a,b), who report critical angles from  $3^{\circ}$  to  $5^{\circ}$  for ice Ih. A lower critical angle would slightly increase the amount of polygonisation. However, lower critical angles reduce numerical stability as the amount of topological errors is increased.

#### Simulation Setup

The simulation setup comprises two numerical strain rates applied to eight model setups with different initial mean grainareas (**Table 1**). Each initial microstructure was discretised in a  $14.14 \times 7.07$  cm box (ratio height/width = 2) and deformed under pure shear conditions to approximately 50% vertical

shortening at incremental strains of 0.5% over 140 time-steps. Different strain rates were achieved by varying the number of recrystallization loops per strain increment. Two or 20 recrystallization loops, per 1.25 · 107s time, per VPFFT strain increment of 0.5%, achieved strain rates of  $2 \cdot 10^{-10} \text{s}^{-1}$  or  $2 \cdot 10^{-11} \text{s}^{-1}$ , respectively. The time step was chosen as a compromise between numerical stability and computational efficiency. The achieved strain rates are higher than reported for the NEEM ice core, where the estimated mean vertical strain rate is  $3.2 \cdot 10^{-12} \text{ s}^{-1}$  (Montagnat et al., 2014). Therefore, the numerical strain rates are only qualitatively comparable with natural strain rates (Steinbach et al., 2016). The temperature in the simulations was set to  $-30^{\circ}$ C, which is comparable to Holocene ice conditions in NEEM ice core (Sheldon et al., 2014). The initial grain sizes were set by varying the initial number of grains in a foam texture (Table 1). The initial c-axis orientations were adjusted to be similar to measured secondorder orientation tensor eigenvalues from NEEM ice core at approximately 700 m depth, defining a weak single maximum CPO which is realistic for many ice cores (see review by Faria et al., 2014a). As summarized in Table 1, the simulations are labeled using a terminology that indicates their mean initial grain area in mm<sup>2</sup> (G) and the order of magnitude in strain rate (R). Hence, for instance the simulation starting with a grain area of 20 mm² at a strain rate of 2  $\cdot$  10<sup>-11</sup> s<sup>-1</sup> is named G20R11.

During the simulations, the numbers of split events by grain dissection and polygonisation is automatically counted for each time-step. As outlined in section Microstructure Discretisation, a grain dissection event during the simulation is defined as a topological event during which two non-neighboring *bnodes* are merged into one. This way, the number of grain dissection and polygonisation events is slightly overestimated. Technically, it is not a grain dissection event when two *bnodes* or grain boundaries close without splitting a grain. The same holds for polygonisation, where all events are counted, including those where a resulting grain is too small and is immediately deleted. Nevertheless, counting split events remains the most reproducible way to estimate the efficiency of grain dissection compared to polygonisation.

To improve statistics, each of the 16 simulations indicated in **Table 1** was repeated three times. For each repetition the initial CPO was slightly varied to allow for some variation between the simulations. The numbers of both polygonisation and grain dissection events for each step were normalized to the actual number of grains at this simulation step. The resulting value can be regarded as the number of events per grain in the respective time-step of the simulation.

# Microstructure Characterisation of NEEM Ice Core Samples

Microstructure and crystallographic-orientation mapping for this study is performed using both EBSD (electron backscatter diffraction) and the automated Fabric Analyser. Using cryo-EBSD, we study three ice core sections from Holocene ice at 442.7, 718.8, and 889.3 m depth and four ice core sections from the glacial ice at 1737.7, 1937.7, 1993.8, and 2103.8 m depth.

Each ice core section of approximately  $90 \times 55 \text{ mm}$  was cut into 10 to 15 EBSD samples using the method of Weikusat et al. (2011a). The samples were imaged by optical microscopy at the Alfred Wegener Institute (AWI) in Bremerhaven before being transported to Utrecht University. All ice core sections, except the ice core section at 442.7 m depth, were mapped using the Nova Nanolab equipped with an EBSD detector (Oxford Instruments HKL Technology, Abingdon, UK) and a cryo-stage (Quorum Technologies Ltd. Ringmer, UK). These EBSD patterns were acquired, processed and indexed using the Channel 5 software of OI-HKL Technology. The ice core section at 442.7 m depth was mapped using a FEI Helios NanoLab G3 UC equipped with the same EBSD detector and cryo-stage. The EBSD patterns of this ice core section were indexed using the Aztec software (Oxford Instruments, High Wycombe, UK). The reader is referred to Weikusat et al. (2011a) for an extensive description of the EBSD sample preparation, sample transfer and the EBSD mapping conditions we used.

A total number of 216 EBSD maps is used for this study, 91 in the Holocene ice and 125 maps in the glacial ice. Depending on the grain size and the area of interest, the EBSD maps vary in area from 0.5 to 6 mm<sup>2</sup>. Each of these EBSD maps was visually checked for signs of grain dissection according to the schematic descriptions of grain dissection by Means (1983), Urai (1983) and Figure 1. A grain dissection event was counted only between second-neighbors with only one grain separating the two dissected grains and if the full orientation difference between the dissected parts was smaller than 3°. The number of grain dissection structures was counted with the area of the EBSD map and its mean grain area. This counting is intended as a qualitative estimate of the frequency of grain dissection in the NEEM ice core. The area of the EBSD map was divided by the observed number of grain dissection events in this map. This provides a measure for the average area necessary to observe one grain dissection event. Afterwards, the average grain size of the EBSD map was divided by this measure resulting in a corrected value. Essentially, this procedure is similar to simply dividing the number of dissection events by the number of grains, but allows correcting for the difference in average grain size, EBSD-map area and for the low number of grains in an EBSD map. We counted completed grain dissection in EBSD maps, which implies that the dissection itself may have occurred in the past and adds a "memory effect" that increases the relative occurrence values. Therefore, the resulting unit is "number of grain dissection events per grain" and can be regarded as the relative chance of a grain being dissected or having been dissected based on the EBSD dataset.

The automated Fabric Analyser (G50 by Russell-Head Instruments) provides high-resolution c-axis-orientation maps of ice thin sections (Wilson et al., 2003). The obtained "c-axis maps" are an essential addition, as they provide better statistics by covering a larger area and, thus, more grains than EBSD maps. Furthermore, more samples per depth can be analyzed (Weikusat and Kipfstuhl, 2010).

For our study, 13 c-axis maps (total area 1.15 m<sup>2</sup> and 8392 grains) from the Holocene part of the NEEM ice core were reviewed to detect grain dissection. In contrast to the EBSD, the Fabric Analyser only provides orientations of the c-axes. This limitation has an effect on the identification of grain dissection events in c-axis maps. Therefore, c-axis maps from the glacial part are not suitable for the search for grain dissection events as c-axis misorientations are too low to identify high-angle boundaries. Furthermore, when 2 s-neighboring grains share the same crystallographic orientation, there is a high probability for them being a product of grain dissection. However, if the full orientation information is missing, such a conclusion may be erroneous.

To avoid erroneously counting grain dissection because of only using c-axis information, we added a grain-connectedness criterion and searched c-axis maps only for grains where grain dissection appeared imminent, but has not yet been completed. For each c-axis map, the number of imminent grain dissection events was counted and divided by the number of grains. Effectively, the result is the same statistical parameter that is derived from EBSD maps, but only for imminent grain dissection events, which results in lower values obtained from c-axis maps than from EBSD maps. One can envisage that more sophisticated ways of determining recent dissection events is possible even in c-axis maps only. However, we did not further explore these and, therefore, the EBSD and c-axis results can so far only be compared qualitatively.

Grain dissection observed in EBSD maps or c-axis maps can potentially be a sectioning effect of a 3D sample. Both methods only show a snapshot of a continuously evolving microstructure, hence an uncertainty remains whether a bulge would have completed the dissection in the third dimension. However, this stereological issue is unproblematic with respect to grain size evolution as grain sizes in ice are also determined from two-dimensional sections (see methods of Binder, 2014). Any interpretation of a natural microstructure is associated with some uncertainty, as it only provides a snapshot of the evolution. Although each counted (imminent) dissection event is not certain, we can assume that the number of interpreted events does correlate with the true number of events.

## RESULTS

### **Numerical Simulation Results**

An overview of selected microstructures after 50% of vertical shortening is shown in **Figure 3**. The final microstructure is marked by curved grain boundaries and only a few equidimensional grains. The c-axes are mainly aligned toward a single maximum CPO as shown by stereographic projections and by common red colors in c-axis azimuth maps. Microstructural similarities are only observed between simulations with common strain rates, independent of initial grain area. As expected, the high strain-rate simulations show smaller final grain areas, whereas the low strain-rate simulations show larger final grain areas. Dislocation densities are higher and more homogeneously distributed at a high strain rate than at a low strain rate.

The circles in Figure 3 represent regions where a splitting of a grain by polygonisation appears imminent. In particular, the grain indicated by circle A in the final microstructure of simulation G10R11 contains two distinct regions with different c-axis azimuth. This grain is expected to split into two grains by polygonisation in the following numerical time-step. Red squares in Figure 3 indicate regions where grain dissection appears either completed (square E) or imminent (squares C and D). Especially square D provides information on the driving force for bulging. Here, two bulges migrate into an area of a grain that exhibits the highest dislocation densities in the microstructure. Close examination of the center of square D reveals high dislocation densities distributed in stripes. The dislocation densities vary strongly locally, also within regions with overall high dislocation densities.

All 16 numerical simulations show situations, during which strongly-bulging grain boundaries migrate through a grain and either merge with the opposite grain boundary or with another bulge (cf. Supplementary Material). Both situations cause splitting of a grain into two parts in the sense of grain dissection. Figure 4 illustrates several examples of grain dissection during the simulations. For example, simulation G15R10 shows a grain boundary bulging into an area of high variation in lattice orientation from step 74 to 84. Ultimately, this bulge migrates through the grain and merges with the opposite boundary. A similar situation is observed in results from simulation G60R10, where a rapidly migrating bulge merges with the opposite boundary, which dissects a grain into two parts. The example from G20R11 illustrates both an event of grain dissection and polygonisation. The bulge indicated by the square migrates toward- and finally merges with the opposite grain boundaries. This dissects the former grain into three parts. The small new grain in the upper left of the bulge shrinks and disappears within the following simulation steps. Furthermore, the bulging grain itself is dissected between simulation step 76 and 80, as visible on the right hand edge of the images. The white ellipse marks a subgrain boundary that develops into a high-angle grain boundary by polygonisation (Figure 4C). All bulges move toward high dislocation-density areas, leaving behind an area free of dislocations. The local dislocation-density field is highly heterogeneous.

Both the low and the high strain-rate simulations with initial grain areas up to  $15 \text{ mm}^2$  are marked by mean grain-area increase (**Figure 5A**). Mean grain-area decrease is observed in high strain rate simulations with initial grain areas higher than 20 mm<sup>2</sup>. The mean grain-area evolutions can be classified in two stages. The first stage up to 30% of vertical shortening is characterized by a regular change in grain area, which either increases or decreases. In the following second stage, an approximate stable mean grain area of  $17 \pm 0.5 \text{ mm}^2$  and  $80 \pm 2.1 \text{ mm}$  is reached in the high and low strain-rate simulations, respectively. Some simulations appear not to have reached a steady state, even at 50% shortening (G80R10 and G60R10; dotted lines in **Figure 5**). Grain-area histograms (**Figure 5B**) show that the grain size distribution broadens with strain from the initial near log-normal distribution.



deformation box. The box is subdivided in the color code for dislocation density (left) and for the c-axes azimuths (**right**), where red colors indicate vertically oriented c-axes. The corresponding pole figures and first eigenvalues of the second order orientation tensor (e<sub>1</sub>) are shown below. The initial pole figure and first eigenvalue of G10R10 are provided as an example of the starting configuration. The squares indicate regions where grain dissection has either occurred or is most likely imminent, while the circles show subgrain boundaries likely to develop into new high-angle grain boundaries by polygonisation.

The number of polygonisation and grain dissection events (**Figure 6**) for each of the eight initial grain-sizes and two strain rates was averaged over the two stages observed in mean grainarea evolution (**Figure 5**). The first stage was taken from step one to 74 (0 to 31% of vertical shortening) and the second one from step 74 to 140 (31 to 50% of vertical shortening). The highest frequencies of both grain dissection and polygonisation events per grain are observed at the low strain rate (left y-axis, black and red symbols in **Figure 6**). Hence, a comparison of their relative frequency is necessary, which is illustrated in the blue curve of **Figure 6** (right y-axis) that shows the percentage of mean grain dissection events from the total mean number of

both grain dissection and polygonisation events per grain. Large errors (standard deviation) for the low strain-rate simulations are a result of the large grain sizes and, therefore small number of grains. In general, the highest fractions of grain dissection events are observed at the high strain rate, although polygonisation generally dominates over grain dissection. However, dissection events dominate when the grain size is close to equilibrium (green dotted lines in **Figure 6**) in the high strain rate experiments. This is observed for small initial mean grain-size simulations already from stage 1 and also for large initial mean grain-size simulations during stage 2. Here, we observe 50% or more split events by grain dissection.



a high-angle grain boundary by polygonisation. (A) Simulation G15R10. (B) Simulation G60R10. (C) Simulation G20R11.

# EBSD and Fabric Analyser Results from NEEM Ice Core

**Figure 7** shows an example of grain dissection in the NEEM core at 718.8m depth. The black spots in the optical microscopy image of **Figure 7A** are air bubbles at or just below the surface (Kipfstuhl et al., 2006). The comparison of this image with the SEM image (**Figure 7B**) shows that the bulge of grain I migrated slightly into grain II during the nine days of sample transport

and storage. The map in **Figure 7D** shows a strong orientation gradient of approximately  $10^{\circ}$  in grain II. Most of this orientation gradient is accommodated by four parallel low-angle (<  $2^{\circ}$ ) subgrain boundaries in grain II. The orientation gradient map indicates a comparatively low misorientation of about 2 to  $3^{\circ}$  between grain III and IV, which is also visible in the schematic illustrations of CPO at positions (a) and (d) in **Figure 7E**.

**Figure 8** shows another example of grain dissection in Holocene ice at 442.7 m depth in the NEEM ice core. The comparison of the optical microscopy image with the SEM image (**Figure 8B**), which was taken eleven days after sample preparation, shows that the surface changed very little during transport and storage at Utrecht University. The EBSD map in **Figure 8C** shows a strong bulge in grain I between grains II and III. Grain II and III differ by about 3° in 3D crystallographic orientation (**Figure 8D**) showing that grain II and III have a very similar CPO (**Figure 8E**). Grain III shows a very low orientation gradient, except for the part close to the bulge of grain II as indicated by the arrow. This low orientation gradient is also reflected in the low misorientations along subgrain boundaries of about 0.5° in this area (**Figure 8C**).

The c-axis maps obtained using the Fabric Analyser were processed manually to detect potential grain dissection events. As described in section 2.2, we selected only events where grain dissection appears imminent and the future fragments are still connected through a thin bridge. **Figure 9** shows a 7 x 9 cm thin section from the NEEM ice core at 1211.7 m depth, grain dissection events are marked by white rectangles. As shown in **Figure 9C**, dissected grains often develop subgrain boundaries across the connecting bridge. This is in agreement with the EBSD data showing high orientation gradients and formation of subgrain boundaries within the dissected grains.

The frequencies of grain dissection events as a function of depth across the Holocene-glacial ice transition are shown in Figure 10. There appears a downward trend toward more dissection events, counted in EBSD images, in the Holocene ice, but with only three samples, this trend may not be significant (Figure 10A). There is, however, a significant decrease in dissection frequencies in the samples from glacial ice, from about one per grain to one per every four grains. Counts of imminent split events observed in c-axis maps are only available for Holocene ice down to 1279 m depth. The average number of imminent split events is much about one per one hundred grains (0.010  $\pm$  0.003). This number is much lower than split events counted in EBSD images as only imminent events are counted in the c-axis maps. The frequencies of grain dissection in c-axis maps do not show a significant trend toward higher or lower grain-dissection frequencies with depth.

## DISCUSSION

### Time-Resolved Numerical Microstructure Evolution under the Influence of Grain Dissection

All simulations show situations that can be identified as grain dissection in the sense of the descriptions by Urai (1987) and



Means (1983, 1989) (see movies, Supplementary Material). The simulations provide a time series to study the interaction of this process with polygonisation, recovery, grain boundary migration and viscoplastic deformation and their relative contribution to microstructure evolution. The numbers of grain dissection and polygonisation events are similar (**Figure 6**), which indicates that both mechanisms significantly contribute to microstructure evolution. Thus, grain dissection cannot be considered as a transient or negligible effect during the simulations, which underlines the necessity to assess its importance for ice micro- to macrodynamics. It needs to be assessed under which boundary conditions such as bulk grain size, strain rate, temperature or stress configuration, grain dissection is most efficient.

Significant numbers of dissection events, compared to the number of polygonisation events, can be seen in the high strain rate simulations (Figures 6A,C). Here, in five of eight simulations, the grain size evolution is marked by grain size decrease, which indicates the grain-size-decreasing character of grain dissection. Additionally, if the grain size does not change significantly from the start or has equilibrated to steadystate values during the second stage of grain size evolution (Figure 5A), grain dissection dominates over polygonisation (Figure 6). In particular, grain dissection is most effective during the second stage of the high strain-rate simulations (**Figure 6C**). The observation of efficient grain dissection at steady-state conditions is consistent with experimental results by Jessell (1986) and Urai (1987). When the mean grain size is larger than the equilibrium one and thus grain size decreases, polygonisation dominates over dissection, as is observed in the high strain-rate simulations and in rock analog experiments by Herwegh et al. (1997).

It remains questionable how suitable mean grain areas are to assess if a steady-state microstructure is reached. Although trending toward more steady values, the final mean grain-areas still vary significantly (**Figure 5A**). The grain area distributions are broadened and more heterogeneous toward the end of the simulations (**Figure 5B**), which is expected from observations of natural ice microstructures under dynamic recrystallization (Kipfstuhl et al., 2009). Obtaining mean grain areas from a broadened grain area distribution can be responsible for the observed variability in final grain areas. Furthermore, at low strain rates, the final number of grains is lowered, which additionally affects the mean grain-area calculation.

The numerical approach is currently limited to 2D simulations. The numerical modeling of processes such as SIBM leading to grain dissection or polygonisation in 3D remains a goal for future developments. In 3D, SIBM can either lead to amoeboidal grains or truly dissected grains (Urai et al., 1986; Figure 25 therein). True dissection in 3D requires bulging along a surface of high dislocation densities. With respect to this, the occurrence of grain dissection can still be expected in 3D. Also the process of 3D polygonisation requires gradients in lattice misorientations and dislocation densities along a surface to develop new high-angle grain boundaries. While the occurrence of polygonisation in natural ice is verified (Alley et al., 1995; De La Chapelle et al., 1998), similar initial structural conditions may as well lead to 3D grain dissection. However, 3D and 2D grain dissection remain slightly different processes. In 3D, grain dissection occurs not at point, but over a period in time during which two boundaries merge. This may cause an overor underestimation of the frequency of grain dissection when being limited to 2D simulations, however, general and qualitative remain valid. For a more quantitative estimate of the frequency of 3D grain dissection in future research, either stereological corrections or 3D numerical simulations are required.

Experimentally observed bulging nucleation (Chauve et al., 2017) can theoretically be modeled with the current numerical resolution. The required processes such as SIBM and subgrain rotation are implemented. However, we do not observe significant bulging nucleation. This may be related to the model resolution, but more likely to the 2D nature of the simulations: With only two dimensions available, splitting off a bulge by necking is unlikely as the region left behind the bulge is strainenergy free. Furthermore, as surface energies tend to straighten



the boundaries and can readily remove small, yet distinct bulges. For efficient bulging nucleation, small bulge widths relative to large grain sizes are required. Under such conditions, we estimate grain dissection less likely as small bulges likely cannot migrate through the whole of a large grain causing dissection, which is consistent with Means (1989). Hence, grain dissection would probably neither be inhibited nor fostered, if bulging nucleation was modeled using higher resolutions.

Compared to natural vertical strain rates at the NEEM ice core that are in the order of  $10^{-12}$  s<sup>-1</sup> (Montagnat et al., 2014), our numerical strain rates are about an order of magnitude higher and results in larger grain sizes than observations in the NEEM ice core (Binder, 2014). Using lower numerical strain rates is feasible, yet even larger grain sizes are produced. The grain size depends on the effective grain boundary mobility that is an Arrhenius-type function of an intrinsic mobility, activation energy and temperature (Nasello et al., 2005). As Steinbach et al. (2016) describe, the numerical setup currently uses literature values for intrinsic grain boundary mobility and activation energy from experimental studies by Nasello et al. (2005). We suggest that the mobility and activation energy are not sufficiently constrained to reproduce realistic grain sizes at natural strain rates. In particular, dissolved impurities are suspected to reduce mobilities (Alley et al., 1986b), but are currently not taken into account in the numerical routine. Further investigations of this issue are beyond the scope of this contribution and remains part of future research.

#### Grain Dissection along NEEM Ice Core

EBSD results on frequencies of grain dissection from **Figure 10A** imply that grain dissection in the NEEM ice core is most efficient in the Holocene ice and in particular around 700–900 meter depth (35–60% estimated finite shortening based on NEEM annual layer thicknesses by Rasmussen et al., 2013). However, whether this trend is real or a result of the limited number of processed samples is uncertain. In particular, this becomes obvious when comparing with results from c-axis maps



(Figure 10B), where no evident trend in the number of imminent grain dissection events is visible.

The results in **Figure 10** can be compared with mean grainboundary curvature data from NEEM ice core presented by Binder (2014, Figures 7.1–7.8 therein). The study by Binder (2014) converts mean grain-boundary curvature to dislocation densities and observes highest curvatures from about 600 to 1300 m depth (30 to 75% estimated finite shortening based on Rasmussen et al., 2013). Our EBSD samples marked by highest relative numbers of grain dissection events are taken from this region of high mean grain-boundary curvature. This implies that strong grain boundary curvature may be indicative for the potential activity of grain dissection. Another characteristic of this region are stable grain sizes (Binder, 2014). The higher efficiency of grain dissection in Holocene ice of NEEM ice core (**Figure 10A**) is in accordance with the observations from simulations that grain dissection is most efficient relative to polygonisation, if the microstructure is in steady state (**Figure 6C**).

The deformation mode in NEEM ice core is interpreted to change from vertical shortening to simple shear at about the transition from Holocene to glacial ice, when c-axes



in Holocene ice trend toward a vertical single maximum (Montagnat et al., 2014). As ice crystals in the Holocene part are mainly vertically shortened, a higher density of non-basal dislocations may be expected in Holocene ice, in particular toward the Holocene-glacial ice transition. The activation of non-basal planes is explicable with the single maximum CPO in which the basal planes are in an unfavorable orientation to accommodate vertical shortening. Alternatively, a constant nonbasal activity would imply a strain rate decrease with depth as the ice becomes harder to deform. Non-basal dislocations provide higher line energies (Schulson and Duval, 2009, pp. 16-18), which in turn implies higher energy gradients driving SIBM and more grain dissection. This may be reflected in Figure 10A showing a trend toward more efficient grain dissection with depth in Holocene ice, but a significantly less grain dissection in glacial ice. Future research could further investigate, whether a change in deformation conditions from pure to simple shear during numerical simulations, will cause similar trends.

## Characteristics of Grain Dissection in Simulation and Nature

Evidence that microstructures exhibit imminent or completed grain dissection events can be found in (1) a distinct distribution of orientation gradients, (2) heterogeneous strain-energy distribution leading to localized occurrence of SIBM, (3) irregular shape of grain boundaries and (4) equal orientations of next-neighbor grains, which Urai (1983) describes as equal orientation families (**Figures 7–9**). Typically, all characteristics (1) to (4) are observed together in natural samples and simulations. Another characteristic important for grain dissection could be (5) the relation of bulge width and mean grain size. The characteristics below can be used as microstructural indicators for the



occurrence of grain dissection. However, we remark that direct evidence is only provided by a time-resolved microstructure evolution.

- (1) Orientation differences indicate high stored strain-energies and can be observed as high densities of subgrain boundaries and orientation gradients. Both EBSD maps, c-axis maps and simulations reveal that grain dissection is accompanied by high orientation gradients (subgrain boundaries) in the dissected grain. The spatial distribution shows these high gradients as high densities of subgrain boundaries on the convex side of bulges (**Figures 4A,C, 9C**). The observation of grain dissection accompanied with subgrain boundaries can be seen as an indication that grain dissection and polygonisation are not completely independent processes but rather act simultaneously, possibly strengthening each other, and cause splitting of grains with high strain-energy gradients.
- (2) Dislocations induce strain energies that drive SIBM. If the dislocation-density difference between the bulging and dissected grain is high, rapid bulge migration is possible (Figure 4, supplementary movies). The direction of grain boundary migration is indicated by locally high orientation gradients that are favorably consumed by the expanding grain (arrow in Figure 8C). In some cases, this direction could be verified using the observed migration of grain boundaries during storage of samples (see dotted line, from

grain I in II, Figure 8B). SIBM causing grain dissection is a localized process as the dislocation energies can be highly heterogeneous within one grain (grain II, Figures 3, 4A,B, 8). Locally high strain energies lead to localized SIBM, which in turn causes directed bulging of grain boundaries and dissection instead of overgrowing of grains. Therefore, localized SIBM may be an essential feature of grain dissection. This assumption is consistent with simulation results, where grain dissection is observed when grain boundaries bulge in areas with locally high dislocation densities (simulation G15R10 in Figure 4). The combination of localized SIBM and grain dissection is further supported by geological studies. For instance, Tullis et al. (1990) observe increased bulging and less polygonisation if the dislocation density distribution is more heterogeneous. The heterogeneous distributions of dislocations in ice are expected, considering that strain localisation is suggested to be a common mechanism in ice micro-dynamics (Jansen et al., 2016; Llorens et al., 2016a; Steinbach et al., 2016). Although these studies describe strain localisation on the scale of polycrystals, their results also show intracrystalline localisation, which is required for localized SIBM and grain dissection. Additionally, Steinbach et al. (2016) indicate that strain localisation may occur over a range of different scales.

(3) The elongated shape of some bulges is caused by strong gradients in stored strain energy and accompanied by



c-axis maps and completed dissection events in EBSD maps.

relatively high orientation gradients. This is reflected between grain I and grain II-III in **Figure 7D** and detail images of simulation G60R10 results (**Figure 4B**). When examining natural microstructures, an irregular grain boundary network and high orientation gradients reflecting strain energy gradients may be indicative for an increased influence of grain dissection.

- (4) Equal orientation of next-neighbor grains or orientation families (grains III and IV, Figure 8C) can only serve as an indication for completed grain dissection if the full CPO (a-axes as well as c-axes) is known. This is the case for EBSD measurements and numerical simulations. However, as a-axes can also align (Miyamoto et al., 2005), even in EBSD-maps, the recognition of orientation families can become difficult when the CPO is very strong. Although an orientation family is clearly observed, other indicators for grain dissection such as an irregular grain boundary network should accompany the observation. Obbard et al. (2006) observed orientation families in GISP2 (Greenland ice sheet project 2) ice core samples. Orientation families may be produced by grain dissection, rather than by polygonisation. In fact, in the misorientation distribution data shown by Obbard et al. (2006), there was no difference between the correlated and un-correlated distributions. This implies that misorientations are controlled by the strong CPO (Fliervoet et al., 1999). In addition, there is a lack of  $5^{\circ}$ -15° misorientation boundaries, which would be expected if polygonisation was the main grain-size-reducing mechanism (Trimby et al., 1998, 2000). The occurrence of a relatively high amount of 5°-15° c-axis misorientations has been suggested as a signature of polygonisation in ice (Alley et al., 1995; Durand et al., 2008). However, the EBSD study of Obbard et al. (2006) shows that c-axis data can overestimate the occurrence of the 5°-15° boundaries.
- (5) The prevalence of grain dissection could be related to grain size itself. Means (1989) shows that grain dissection is most frequent when mean grain size and bulge width are similar. We can identify three situations (a-c) to describe this dependency: (a) If the grain size is significantly larger, a bulge will remain close to the position of the original boundary and does not migrate through a grain. In this situation, grain dissection is not possible. (b) On the other hand, if the grain size is significantly smaller than the bulge width, the bulge shape itself cannot develop and the migrating boundary consumes a whole grain instead of dissecting it. (c) Dissection and resulting grain-size reduction is only possible when bulges are about half a grain diameter wide. Our results appear to support these dependencies. In NEEM glacial ice, the grain size is smaller and grain dissection is less common than in Holocene ice (Figure 10A). In our simulations, the frequency of grain dissection was higher for high strain rate simulations leading to smaller grain sizes (Figure 6). This may illustrate the two end-members of grain size being larger (NEEM glacial ice) or smaller than the bulge width (simulations at low strain rate). A further investigation and quantification of such dependencies should form part of future studies on grain dissection.

It was argued above that grain dissection is more important when the grain size is close to steady state than at either smaller or larger grain sizes. Although grain dissection is most significant at this grain size, polygonisation events may still outnumber grain dissection events. Therefore, we interpret that with such equilibrium conditions, suitable bulge width as described above (situation 5c) are achieved through a combination of polygonisation and SIBM. A steady state is only reached when deformation conditions are stable. High frequencies of dissection events can thus be regarded as indicators for relatively constant conditions. This appears to fit the observations in the NEEM ice core, where high frequencies of grain dissection are found at the base of the Holocene ice (Figure 10A). While microstructures stabilize downward in Holocene ice, both the CPO (Montagnat et al., 2014) and the grain size (Binder, 2014) change at the transition to glacial ice. According to the recrystallization diagram by Faria et al. (2014b), this change reflects a change in deformation conditions. In turn, this implies less grain dissection relative to polygonisation, which seems to fit our observation of low frequencies in grain dissection in glacial ice (Figure 10A).

The proposed mechanisms controlling grain sizes in ice are classically polygonisation (Alley et al., 1995; De La Chapelle et al., 1998) or bulging nucleation (Montagnat et al., 2015; Chauve et al., 2017) leading to decreasing grain sizes and grain boundary migration leading to a grain size increase (Duval and Castelnau, 1995; De La Chapelle et al., 1998). A mixture of both is suspected to cause steady grain sizes in the middle of ice-sheets columns. However, SIBM may provide an additional grain-size-reducing process, if grain dissection is initiated (Means, 1989). Therefore, equilibrium grain sizes may be achieved with only SIBM, whereas polygonisation or nucleation need additional grain-size-increasing mechanisms to achieve equilibrium.

## CONCLUSIONS

In this study, we investigate the importance of grain dissection as a feature of strain-induced boundary migration (SIBM) in ice using numerical simulations and natural microstructures from the NEEM ice core. For the first time, we present evidence that grain dissection is a common mechanism during ice deformation. The efficiency of grain dissection is probably independent of depth and rather a function of the state of the microstructure and deformation conditions. In particular, grain dissection is most efficient in depths in the ice column where deformation conditions remained constant over time and microstructures approach steady state in terms of grain size or CPO. Here, grain dissection is an efficient mechanism in addition to polygonisation, to achieve grain size reduction and maintain a balance between grain-size-increasing anddecreasing mechanisms. In turn, this implies that SIBM not necessarily leads to grain size increase, but eventually to the dissection of grains, especially at high strain energy gradients.

Future models that describe grain-size evolution during ice deformation, should incorporate grain dissection and further investigate its frequency as a function of grain size, deformation

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mode, CPO or other microstructural properties. This should lead to a parameterisation of grain dissection, which forms the precursor for including the process in a grain-size sensitive ice flow law required to describe large-scale ice flow.

### **AUTHOR CONTRIBUTIONS**

Initial concept by FS and EK. FS performed numerical modeling with support from AG and PB. EK did electron backscatter diffraction analyses supported by MD and GP. JE processed the Fabric Analyser data. IW provided the glaciological input, samples and NEEM Fabric Analyser measurements. Major parts of the paper were written by FS, EK and JE with contributions of all co-authors.

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## DATA AVAILABILITY

The video supplement related to this article is available online on figshare.com: https://doi.org/10.6084/m9.figshare.5160997.v1 (Steinbach et al., 2017).

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**Conflict of Interest Statement:** The authors declare that the research was conducted in the absence of any commercial or financial relationships that could be construed as a potential conflict of interest.

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